## Software tutorial/Integration of ODEs

From Process Model Formulation and Solution

< Software tutorial

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# Background

In our course we have learned several ways of integrating a single equation  $\frac{dy(t)}{dt} = f(t, y)$  with a given initial condition  $y(t = 0) = y_0$ ; and we have shown that a system of n first order ODE's can be integrated:

$$\frac{d\mathbf{y}(t)}{dt} = \mathbf{f}(t,\mathbf{y})$$

given a set of n initial conditions  $\mathbf{y}(t=0) = \mathbf{y}_0$ , i.e.  $\mathbf{y}_0$  is an n imes 1 vector. The course notes covered Euler's method, Heun's method and Runge-Kutta methods.

However, we only coded Euler's method (because it was simple!), but not the others. These other methods have been (reliably) coded in software packages and sophisticated error correction tools built into their algorithms. You should always use these toolbox functions to integrate your differential equation models. In this section we will show how to use MATLAB and Python's built-in functions to integrate:

a single differential equation

a system of differential and algebraic equations.

We will only look at initial value problems (IVPs) in this tutorial.

### MATLAB

 $MATLAB's has several ODE solvers available (http://www.mathworks.com/help/techdoc/ref/ode45.html) . You can read up more about the implementation details in this technical document (http://www.mathworks.com/help/pdf_doc/otherdocs/ode_suite.pdf) .$ 

#### Python

Like MATLAB, several integrators are available in Python. The integrator I will use in this tutorial is one of the most recent additions to SciPy - the VODE integrator (https://computation.llnl.gov/casc/nsde /pubs/207532.pdf) developed at Lawrence Livermore National Laboratories in 1988. It is a good general-purpose solver for both stiff and non-stiff systems.

NOTE: we will use the superior vode Python integrator - it requires a little more code than the other built-in Python integrator, based on lsodea.

## **Example problem**

The example we will work with is a common modelling reaction: a liquid-based stirred tank reactor, with (initially) constant physical properties, a second order chemical reaction where species A is converted to B according to  $A \rightarrow B$ , with reaction rate  $r = kC_A^2$ . One can find the time-dependent mass balance for this system to be:

$$rac{dC_{\mathsf{A}}(t)}{dt} = rac{F(t)}{V} \left( C_{\mathsf{A},\mathrm{in}} - C_{\mathsf{A}} 
ight) - kC_{\mathsf{A}}^2$$

where  $C_{A,in} = 5.5 \text{ mol/L}$ , we will initially assume constant volume of V = 100 L and constant inlet flow of F(t) = 20.1 L/min. The reaction rate constant is  $0.15 \frac{\text{L}}{\text{mol.min}}$ . We must specify an initial condition for every differential equation: we will let  $C_A(t = 0) = 0.5 \text{ mol/L}$ .

In the code below we will integrate the ODE from  $t_{
m start}=0.0$  minutes up to  $t_{
m final}=10.0$  minutes and plot the time-varying trajectory of concentration in the tank.

MATLAB	Python
In a file called tank.m:	import numpy as np
<pre>function dydt = tank(t, y)</pre>	<pre>from scipy import integrate from matplotlib.pylab import *</pre>
<pre>% Dynamic balance for a CSTR %</pre>	<pre>def tank(t, y):     """</pre>
$ \  \  \  \  \  \  \  \  \  \  \  \  \ $	Dynamic balance for a CSTR
<pre>% Returns dy/dt = F/V*(C_{A,in} - C_A) - k*C_A^2</pre>	$C\_A$ = y[0] = the concentration of A in the tank, mol/L
F = 20.1; % L/min	Returns $dy/dt = F/V*(C_{A,in} - C_A) - k*C_A^2$
CA_in = 2.5; % mol/L	
V = 100; % L	F = 20.1 # L/min
k = 0.150; % L/(min.mol)	CA_in = 2.5 # mol/L
	V = 100 # L
<pre>% Assign some variables for convenience of notation CA = y(1);</pre>	k = 0.15  # L/(mol.min)
	# Assign some variables for convenience of notation
% The output from the ODE function must be a COLUMN vector, % with n rows	CA = y[0]
<pre>n = numel(y); % How many ODE's in this system?</pre>	# Output from ODE function must be a COLUMN vector, with n rows
dydt = zeros(n, 1);	<pre>n = len(y) # 1: implies its a single ODE</pre>
$dydt(1) = F/V^*(CA_in - CA) - k^*CA^2;$	<pre>dydt = np.zeros((n,1))</pre>
	$dydt[0] = F/V^*(CA_in - CA) - k^*CA^{**2}$
¥	return dydt
In a separate file (any name), for example: ode_driver.m, which will "drive" the ODE	I The Made and Alexandra the OPE (a)
solver:	# ine driver that will integrate the ODE(s):
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The reason for the longer Python code is because we have to constructe the vectors that store the time variable and the corresponding concentration output (as a function of that time variable). The MATLAB code builds this vector for us. MATLAB's vectors are very well suited to plotting, but there is a feature that may not be 100% useful:

MATLAB	Python
Let's take a look at the MATLAB output:	Let's take a look at the Python output:
<pre>&gt;&gt; t(1:10) ans =</pre>	>>> t[0:10] array([[ 0. ], [ 0.1], [ 0.2], [ 0.3], [ 0.4], [ 0.5], [ 0.6], [ 0.6], [ 0.7], [ 0.8], [ 0.9]])
<pre>&gt;&gt; y(1:10) ans =</pre>	array([[ 0.5 ], [ 0.53581076], [ 0.57035065], [ 0.60362937], [ 0.63566104], [ 0.66646269], [ 0.69605419], [ 0.7244578 ], [ 0.75169755], [ 0.77779875]]
MATLAB places the points at unequal step sizes of time. This is what their documentation has to	The evenly spaced periods of time were by design - see the Python code above. After reading the MATLAB description alongside, you might think the Python integration is inaccurate. This is not true: the Python code we have used here will take multiple steps, of variable size, within each of

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the delta\_t time steps we specified, but the code will only report the values at the boundaries of each delta\_t, not the intermediate values.

The MATLAB ODE solvers utilize these methods by taking a step, estimating the error at this step, checking to see if the value is greater than or less than the tolerance, and altering the step size accordingly. These integration methods do not lend themselves to a fixed step size. Using an algorithm that uses a fixed step size is dangerous since you can miss points where your signal frequency is greater than the solver frequency. Using a variable step ensures that a large step size is used for low frequencies and a small step size is used for high frequencies. The ODE solvers within MATLAB are optimized for a variable step, run faster with a variable step size, and clearly the results are more accurate.

### **Example with coupled ODEs**

We will now expand our example to a system of two coupled ODEs. Still in the same reactor we are now considering the rate constant to be a function of temperature:  $k = 0.15e^{-E_a/(RT)}$ L/(mol.min), with  $E_a = 5000$  J/(mol) and R = 8.314 J/mol.K, and T(t) is the time-varying tank temperature, measured in Kelvin. Furthermore, the reaction is known to release heat, with  $\Delta H_r = -590$  J/mol. The time-dependent mass and energy balance for this system is now:

$$rac{dC_{\mathsf{A}}(t)}{dt} = rac{F(t)}{V}\left(C_{\mathsf{A},\mathrm{in}} - C_{\mathsf{A}}
ight) - 0.15e^{-E_{\mathrm{a}}/(RT)}C_{\mathsf{A}}^2 
onumber \ rac{dT(t)}{dt} = rac{F(t)
ho C_p(T)}{V
ho C_p(T)}\left(T_{\mathrm{in}} - T(t)
ight) - rac{0.15e^{-E_{\mathrm{a}}/(RT)}C_{\mathsf{A}}^2V(\Delta H_r)}{V
ho C_p}$$

where  $C_{A,in} = 2.5 \text{ mol/L}$ ,  $T_{in} = 288 \text{ K}$ ; we will initially assume constant volume of V = 100 L and constant inlet flow of F(t) = 20.1 L/min. Also,  $C_p(T) = 4.184 - 0.002(T - 273)$ J/(kg.K), the molar heat capacity of the liquid phase system, a weak function of the system temperature. The density of the liquid phase is  $\rho = 1.05 \text{ kg/L}$ . We need two initial conditions as well:

• 
$$C_{\sf A}(t=0) = 0.5 \, {
m mol/I}$$

• 
$$T(t=0) = 295K$$

say:

In the code below we will integrate the ODE from  $t_{start} = 0.0$  minutes up to  $t_{final} = 45.0$  minutes and plot the time-varying trajectory of concentration in the tank.

MATLAB	Python
I ne following code appears in an m-file called: tank_coupled.m	
	import numpy as np
function dudt $= tank coupled(t = u)$	from scipy import integrate
$runction ayat = tank_couplea(t, y)$	from matplotlib.pylab import *
& Dynamic balance for a CSTR	dof topk (t v)
$^{\circ}$ C A = v(1) = the concentration of A in the tank. [mol/L]	
S = V(2) = the tank temperature. [K]	Dynamic balance for a CSTR
8 8	bynamie baranee for a cork
<pre>% Returns dv/dt = [F/V*(C {A, in} - C A) - k*C A^2]</pre>	C A = v[0] = the concentration of A in the tank. [mol/L]
<pre>% [F/V*(T in - T) - k*C A^2*HR/(rho*Cp) ]</pre>	T = v[1] = the tank temperature. [K]
90°	
	Returns $dy/dt = [F/V*(C_{A,in} - C_A) - k*C_A^2]$
F = 20.1; % L/min	[F/V*(T_in - T) - k*C_A^2*HR/(rho*Cp) ]
CA_in = 2.5; % mol/L	нин
V = 100.0; % L	F = 20.1 # L/min
k0 = 0.15; % L/(mol.min)	CA_in = 2.5 # mol/L
Ea = 5000; % J/mol	V = 100.0 # L
R = 8.314; % J/(mol.K)	k0 = 0.15 # L/(mol.min)
Hr = -590; % J/mol	Ea = 5000
T_in = 288; % K	R = 8.314 # J/(mol.K)
rho = 1.050; % kg/L	Hr = -590 # J/mol
	T_in = 288 # K
% Assign some variables for convenience of notation	rho = 1.050 # kg/L
CA = y(1);	
T = y(2);	# Assign some variables for convenience of notation
9. Alexandria americana	CA = y[0]
* Algebraic equations	$T = \gamma[T]$
$K = K0^{\circ} \exp(-Ed/(K^{-1})); \leq L/(mot.min)$	
$Cp = 4.184 - 0.002^{\circ}(1-275), + 57(kg.k)$	# Algebraic equations
& The output from the ODE function must be a COLUMN vector	$K = KU \wedge np.exp(-Ea/(R^{-1})) \# L/(mol.mln)$
% with n rows	$Cp = 4.184 = 0.002^{\circ}(1-273) \# 07(Kg.K)$
n = numel(v): % How many ODE's in this system? 2	# Output from ODE function must be a COLUMN vector with p rows
dvdt = zeros(n, 1);	n = len(y) # 2: implies we have two ODEs
$dydt(1) = F/V^*(CA_in - CA) - k^*CA^2;$	dvdt = np.zeros((n, 1))
$dydt(2) = F/V^{*}(T_in - T) - (Hr^{*}k^{*}CA^{2})/(rho^{*}Cp);$	$dydt[0] = F/V^*(CA in - CA) - k^*CA^{**2}$
	$dvdt[1] = F/V^{*}(T \text{ in } - T) - (Hr^{*}k^{*}CA^{**2})/(rho^{*}Cp)$
	return dydt
In a separate file (any name), for example: ode_driver.m, which will "drive" the ODE	-
solver:	<pre># The ``driver`` that will integrate the ODE(s):</pre>
	<pre>ifname == 'main':</pre>
% Integrate the ODE	# Start by specifying the integrator:
° −−−−−−−−−	<pre># use ``vode`` with "backward differentiation formula"</pre>
	<pre>r = integrate.ode(tank).set_integrator('vode', method='bdf')</pre>
% Set the time range:	
t_start = 0;	# Set the time range
t_final = 45.0;	t_start = 0.0
	t_final = 45.0
% Set the initial condition(s):	uerca_t = U.1
CA_t_zero = 0.5;	# Number of time steps: I extra for initial condition
1_t_zero = 295;	num_steps = np.rioor((t_rinar = t_Start)/defta_t) + 1
& Integrate the ODE(a).	# Set initial condition(s) for integrating variable and time!
$\circ$ integrate the ODE(s):	CA + zero = 0.5
[c, y] = oue+s(@tdlik_Coupied, [t_Stdft, t_iiidi],	T + zero = 295.0
[CA_L_2010, 1_L_2010]),	r.set initial value([CA t zero, T t zero], t start)
& Plot the results.	
clf:	# Additional Python step: create vectors to store trajectories
subplot (2, 1, 1)	t = np.zeros((num_steps, 1))
plot(t, v(:, 1))	CA = np.zeros((num_steps, 1))
	<pre>temp = np.zeros((num_steps, 1))</pre>

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fig.savefig('coupled-ode-Python.png')

The trajectories produced by the above code are shown below. Do they make engineering sense?



Important notes

- Each trajectory (ODE) must have an initial condition.
- The function that specifies the ODE must return a *column* vector with n entries, one for each ODE. Algebraic equations may be included in the ODE function. For example:  $C_p = 4.184 0.002(T 273)$  is an algebraic function

  - If the inlet flow varied over time according to  $F(t)=20.1+2\sin(t)$  then this algebraic equation could be added.
- Numerical integration allows for discontinuities. For example, a step input at t=50 minutes in the inlet flow can be coded as

if t < 50 F = 20.1else F = 25.1end

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