



Position Pickups for the Cryogenic Storage Ring

Felix Laux

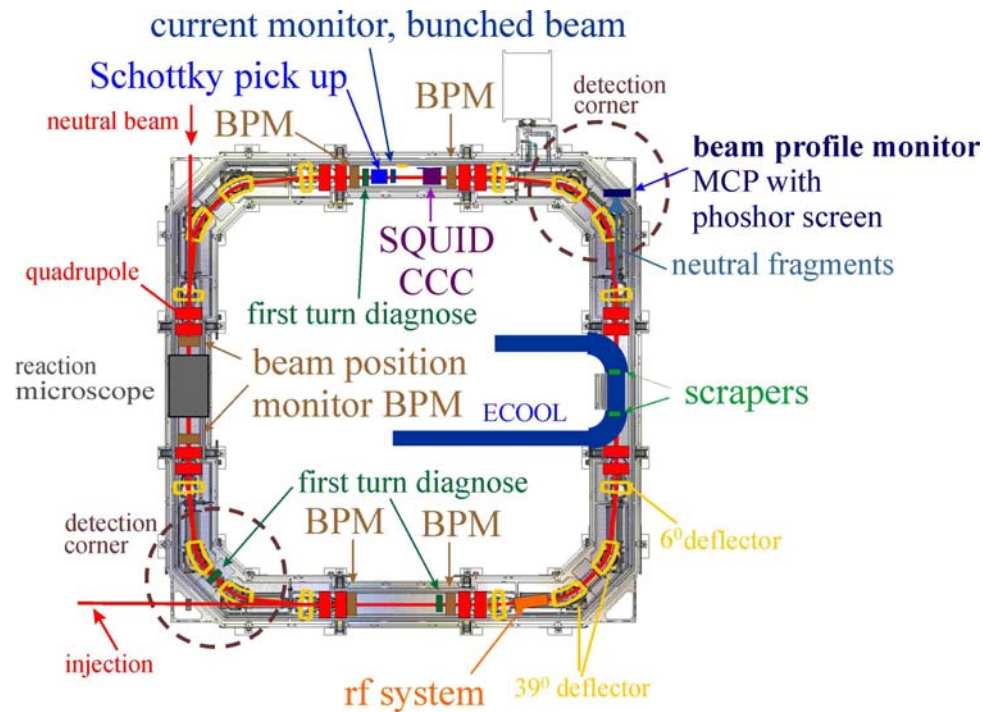
Low Current, Low Energy Beam
Diagnostics Workshop

Hirschberg 23.11.09 - 25.11.09





Position Pickups at CSR

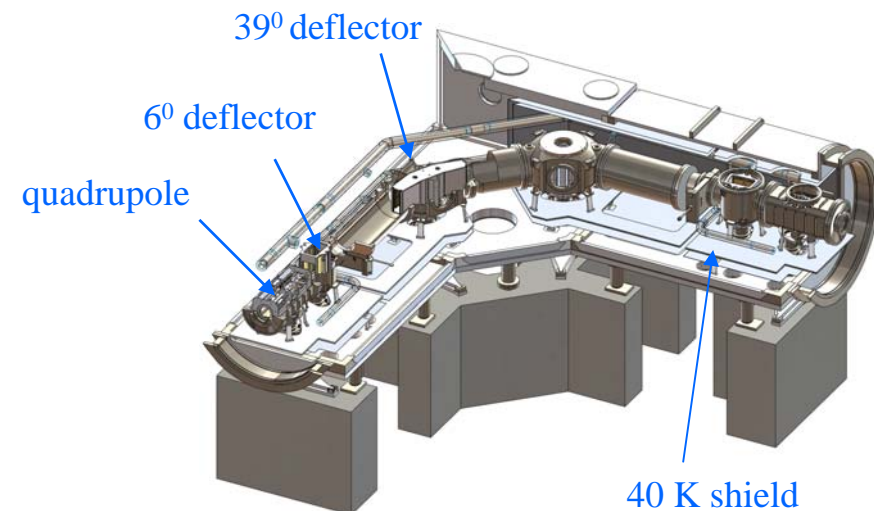


- closed orbit measurements, alignments of beam to experiments
- Beam Transfer Function / tune
- limited possibility of first turn diagnostics



Problem statement

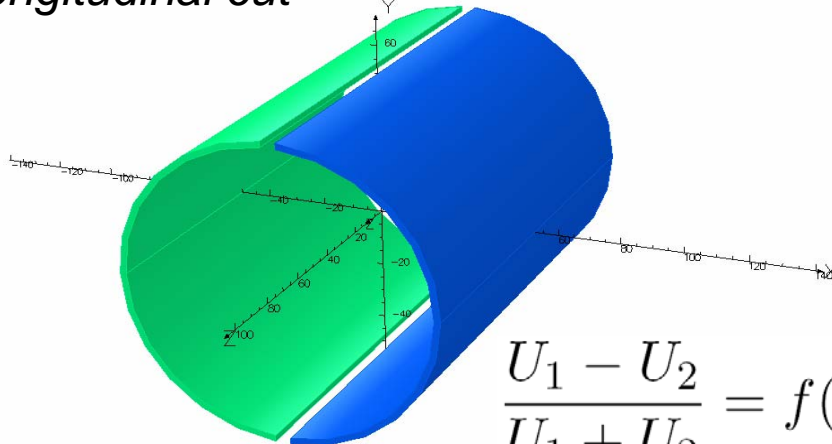
- Measure center of charge of the beam to < 0.5 mm precision
 - Beam currents: 1 nA – 1 μ A
 - Ion mass: 1-100 amu
 - Energy range (1^+ ions): 20 – 300 keV
- Frequencies 5 – 200 kHz
- Measurements with uncooled beams should be possible (no higher harmonics)
 - Absolute position accuracy < 0.5 mm





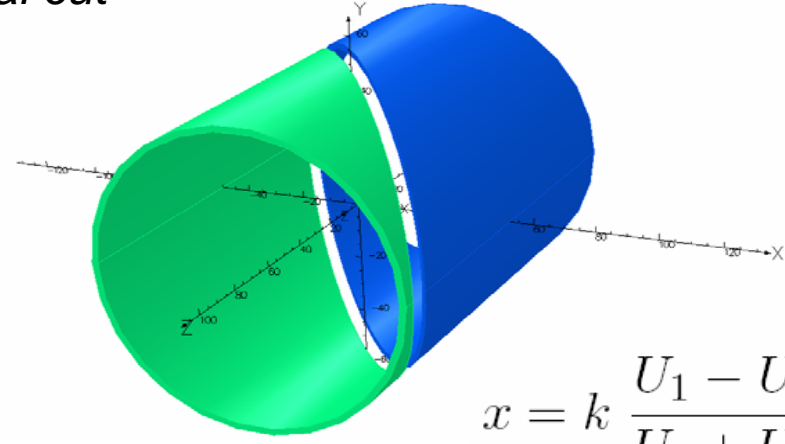
Comparison between longitudinally and diagonally slit pickups

Longitudinal cut



$$\frac{U_1 - U_2}{U_1 + U_2} = f(x, y)$$

Diagonal cut



$$x = k \frac{U_1 - U_2}{U_1 + U_2}$$

- Electrode shape – longitudinally or diagonally cut
- Beam Position Monitor vs. multi-purpose device
- Comparison of Δ/Σ for beams with 2 mm and 25 mm diameter located at $x=25$ mm and $y=0$ mm.

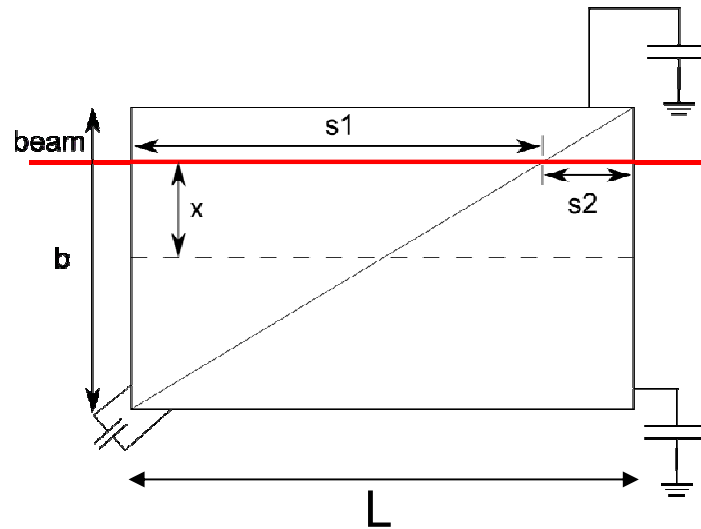
Diagonally cut pickup: no change in scaling factor

Longitudinally cut pickup: position dependance of scaling factor causes a systematic measurement error of $\Delta x=0.05$ mm.



Scaling factor of diagonally slit pickups

$$I_s = \omega I_b \Delta t$$
$$\rightarrow I_s = \omega I_b \frac{L}{v}$$



$$x = k \frac{U_1 - U_2}{U_1 + U_2}$$

$$k = (1 + 2 C_k / C) b / 2 \longrightarrow C_k = 6 \text{ pF}, C = 60 \text{ pF} : k = 60 \text{ mm}$$

Example:

1 nA H⁺-beam, $f_0 = 200$ kHz,

$L = 8$ cm, $v = 0.025 c$

$$U_1 + U_2 = \frac{1}{C} I_b \frac{L}{v} = 180 \text{ nV}$$

$$x = 0.5 \text{ mm} \longrightarrow \Delta U = 1.5 \text{ nV}$$



Measurement frequency

- Capacitive pickups can measure position of bunched beam only!

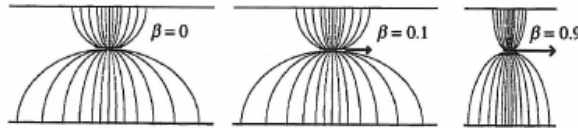
If beam coasts at frequency f , choose $h \times f$ to bunch the beam

$$f_0 = \frac{1}{2\pi} \frac{1}{\sqrt{LC}}$$

Mass range	1-100 amu
Energy range (1^+ ions)	20 - 300 keV
Frequency range	5 kHz - 200 kHz
Intensity range	1 nA - 1 μ A

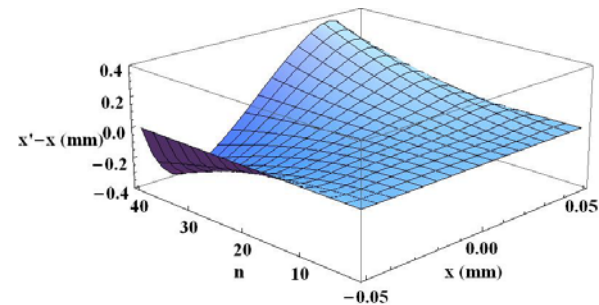
- Keep losses low due to L
- Required frequency shift should not be too high
→ Choose a frequency range much higher than the range of frequencies of the coasting beam!

But!



Low- β effect

Cannot bunch to too high harmonics ($h < 40$)!
Chose 200 – 400 kHz as appropriate



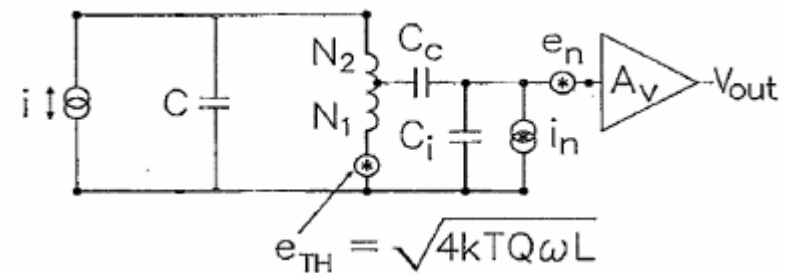
Systematic error due to the low- β effect



Calculation of the Signal-to-Noise ratio

Sources of noise:

- Thermal noise: $U_n = \sqrt{4 k T Z}$
- Voltage noise of amp: E_n
- Current noise of amp: $I_n Z$



Impedances:

$$Z_{\text{non-resonant}}(\omega) = \frac{1}{\omega C}$$

$$Z_{\text{resonant}}(\omega = \omega_0) = \frac{Q}{\omega C}$$

$$\alpha = \frac{N_1}{N_1 + N_2} \frac{C_c}{C_c + C_i}$$

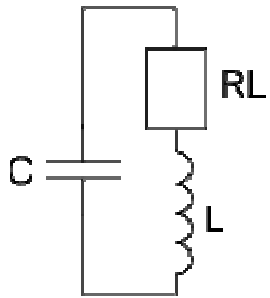
S/N optimized if: $\frac{E_n}{I_n} = Z_{\text{source}}$

$$S/N = \sqrt{\frac{I_s^2 Z^2}{(4 k T Z + I_n^2 Z^2 \alpha^2 + E_n^2 / \alpha^2) \Delta f}}$$



Inductance

Impedance at resonance



$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$Z(\omega = \omega_0) = \frac{1}{R_L} \frac{L}{C}$$

Capacity budget

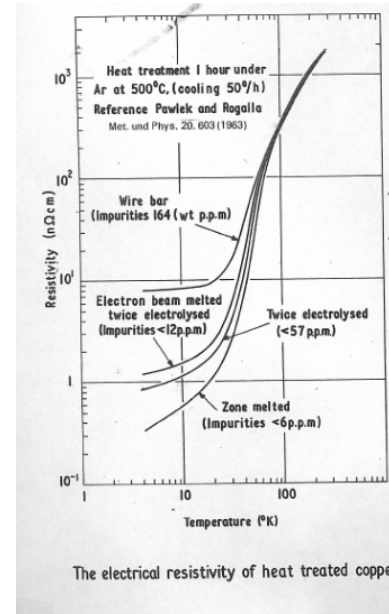
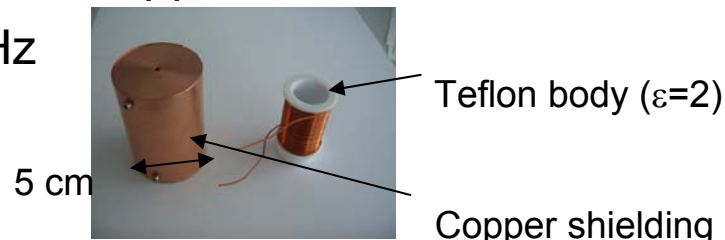
element	C [pF]	source
electrode	20	Tosca calculation
feedthrough ¹	5	estimate
switches (relays)	2.5	datasheet
cables	?	
coil	10	estimate
variable capacity diode	5	datasheet
amplifier	15	data sheet/estimate

Coils made from copper wire

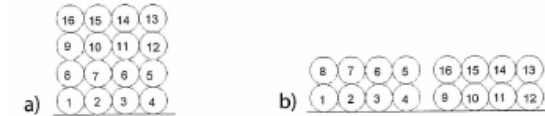
C=70 pF, 400 kHz

→ L=2.2 mH

→ N~400



Reduction of capacity by chamber winding



Examples (H. Kracke):
Copper coil,
L=2.2 mH, Cs=8.3 pF,
RL=22 Ohm @ 4K

→ Q = 250 (400kHz)

- RRR=66
- Coupling to resonator probably to strong

$$R_{Coil} \approx \frac{\rho l}{2 \pi r \delta}, \quad \delta = \sqrt{\frac{2 \rho}{\mu \omega}}$$

Superconducting coil (copper shielding), RL=5 Ohm @ 4K

→ Q = 1100 (400kHz)

Superconducting coil (super cond. shielding), RL=1.7 Ohm @ 4K

→ Q = 3300 (400kHz)

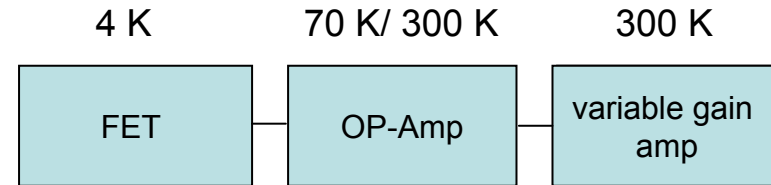
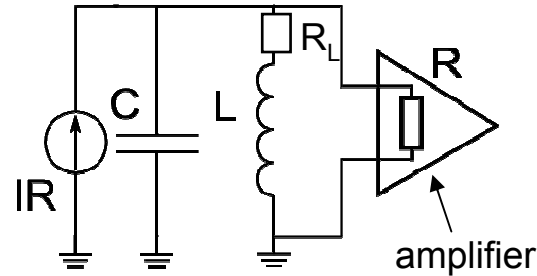




Cryo-amplifiers

Use cryo-amplifiers to be as close as possible to signal source!

Q	$Z(M\Omega)$
250	1.4
1100	6.1
3300	18.5



Requirements

- DC input impedance high enough to not to lower quality factor
- Low Voltage noise
- Very low Current noise
- Cryo-capable
- Low power consumption

Example data of comm. available amplifier

- $R=22.7\text{ M}$
- $E_n=8\text{ nV}/\sqrt{\text{Hz}}$
- $I_n=8\text{ fA}/\sqrt{\text{Hz}}$
- GaAs-Technology
- 10 mW

GaAs FET cryo-capable!



Benefits from Resonant Amplification (I)

Noise

	Q	$Z(M\Omega)$	U_n (nV)	E_n (nV)	$I_n Z$ (nV)	Total Noise (nV)
resonant	250	1.4	175	80	111	222
	1100	6.1	367	80	489	617
	3300	18.5	630	80	1438	1572

$f=400$ kHz

RBW=100 Hz

non-resonant

$$Z_{\text{non-resonant}} \approx \frac{1}{\omega C} = 5.6 \text{ k}\Omega$$

$$U_n=11 \text{ nV}, E_n=80 \text{ nV}, I_n Z=0.4 \text{ nV}, \text{ Total Noise}=80.7 \text{ nV}$$

Signal

$$I_s = \omega I_b \Delta t$$

Beam current
to signal current
calculation

$$\rightarrow I_s = \omega I_b \frac{L}{v}$$

$$\rightarrow I_s = 2 \pi h I_b \frac{L}{C_0}$$

$$h = 1 \rightarrow I_s/I_b = 2 \pi \frac{L}{C_0} = 1.4\%$$

$$f=400 \text{ kHz}, h=20, Q=250, l=0.08 \text{ m}, C_0 = 35 \text{ m}, I_b = 1 \text{ nA}$$

$$U_{\text{resonant}}=200 \mu\text{V} \rightarrow \text{S/N}=59 \text{ dB}$$

$$U_{\text{non-resonant}}=0.8 \mu\text{V} \rightarrow \text{S/N}=20 \text{ dB}$$

S/N improvement 39 dB





Benefits from

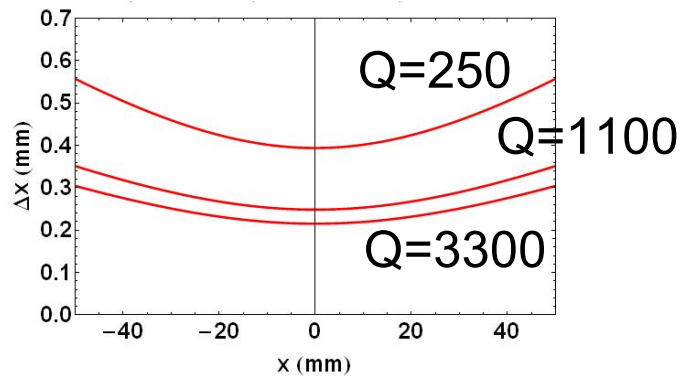
Resonant Amplification (II)

$$x = k \frac{U_1 - U_2}{U_1 + U_2} \rightarrow \Delta x = k \sqrt{\left(\frac{2 U_2}{(U_1 + U_2)^2} U_{\text{noise}}\right)^2 + \left(\frac{-2 U_1}{(U_1 + U_2)^2} U_{\text{noise}}\right)^2}$$
$$\Delta x < 0.25 \text{ mm} \rightarrow S/N > \frac{2 k}{\Delta x} = 400, f = 400 \text{ kHz}, h = 2 \rightarrow Q = 1100$$

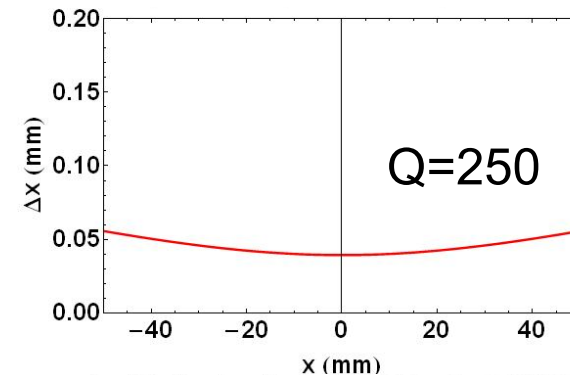
Position dependence of position error

resonant

$I_b = 1 \text{ nA}$,
 $f = 400 \text{ kHz}$,
 $h = 2$,
 $\alpha = 1$,
 $\Delta f = 100 \text{ Hz}$

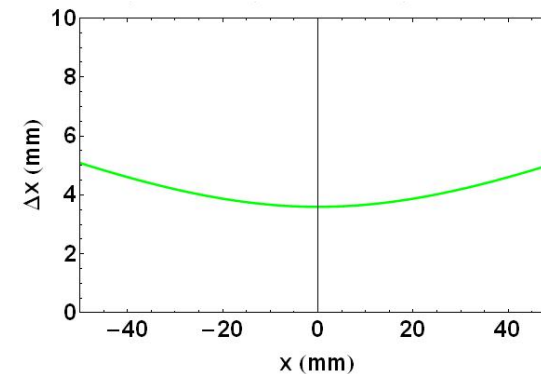
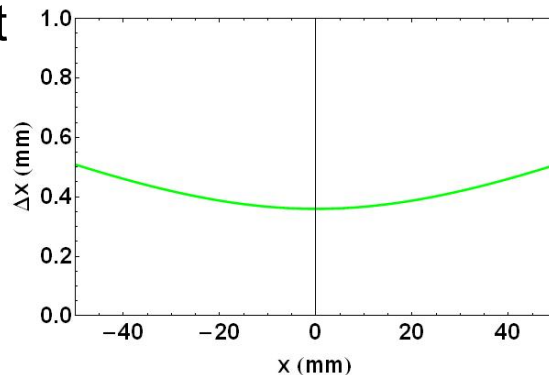


$I_b = 1 \text{ nA}$,
 $f = 400 \text{ kHz}$,
 $h = 20$,
 $\alpha = 1$,
 $\Delta f = 100 \text{ Hz}$



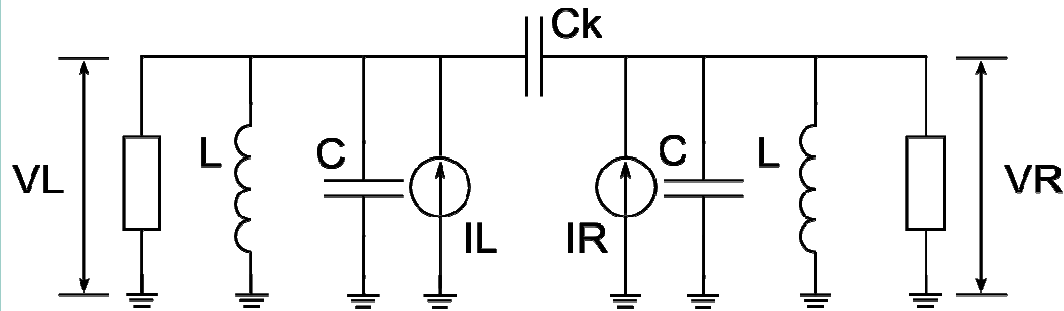
non-resonant

$I_b = 0.1 \mu\text{A}$,
 $f = 400 \text{ kHz}$,
 $h = 2$,
 $\alpha = 1$,
 $\Delta f = 100 \text{ Hz}$

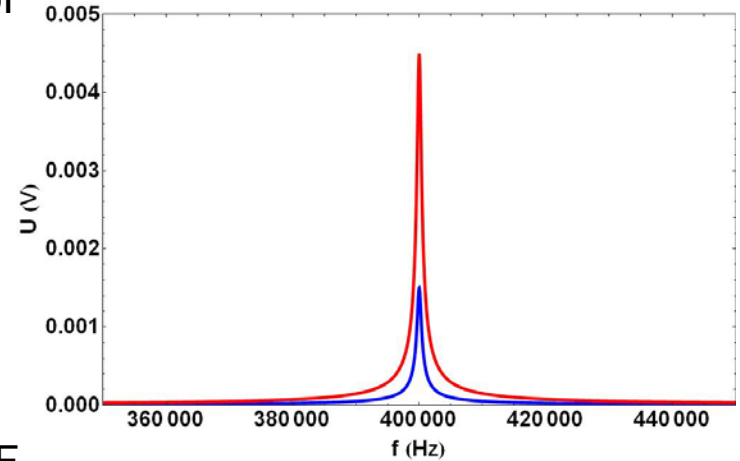




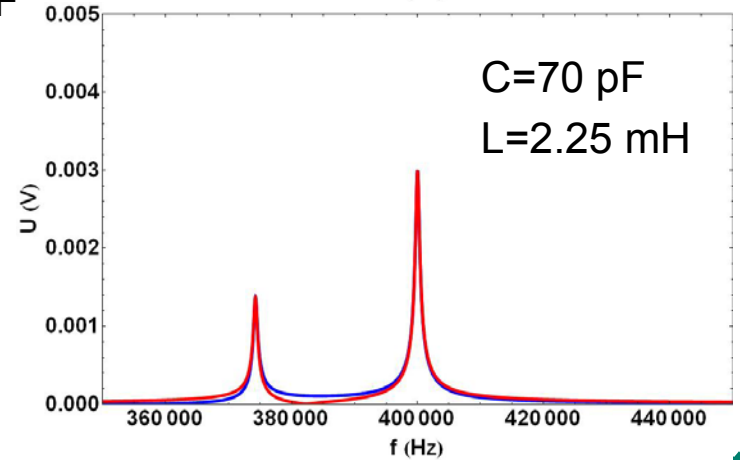
Effects of coupling



$C_k = 0 \text{ pF}$

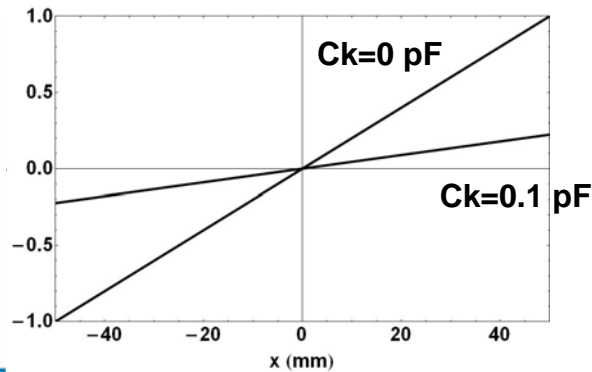
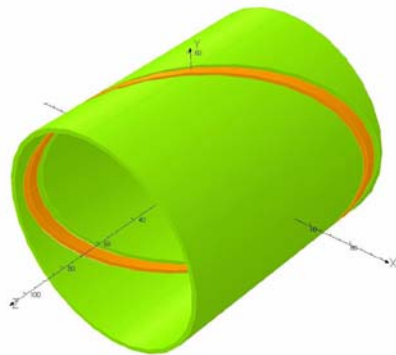


$C_k = 5 \text{ pF}$



Guard Ring: $6 \text{ pF} \rightarrow 4 \text{ pF}$

Not sufficient!

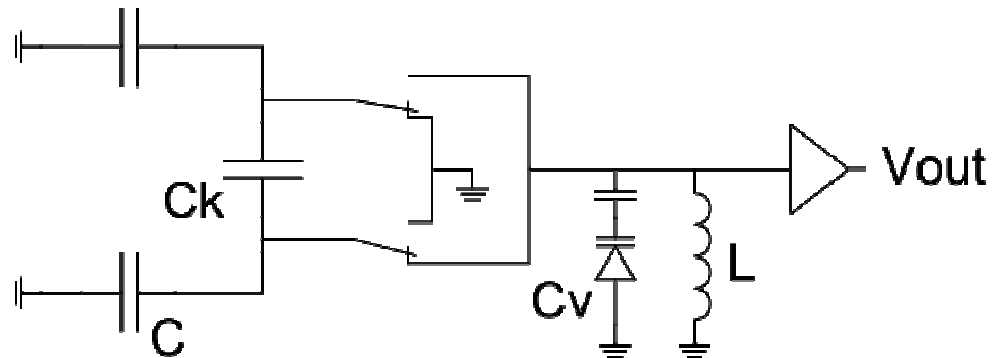


Opera



Amplification circuit

@ 300 K	GaAs FET Switch	HF Relay
On resistance	3.9 Ω	0.2 Ω
Off resistance	200 k Ω	10 ¹⁰ Ω
Capacity	15 pF	2.5 pF
Life time (cycles)	–	100 10 ⁶
Switching time	4 ns	1 ms
State hold power	6.4 mW	32 mW

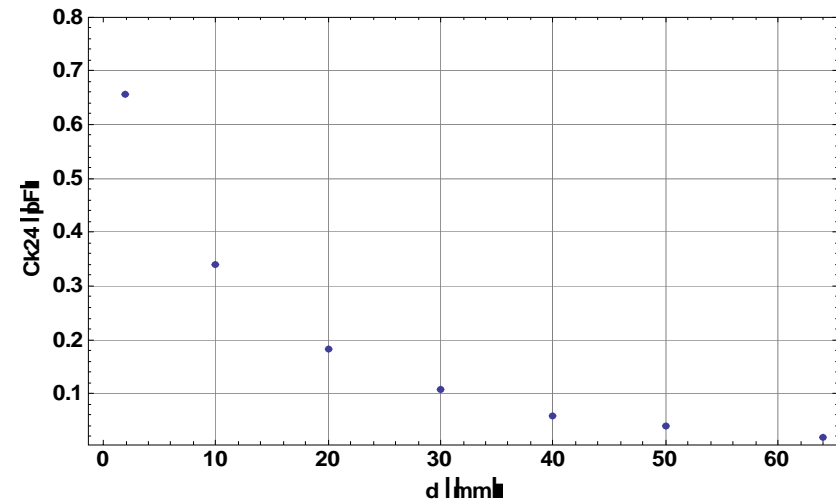
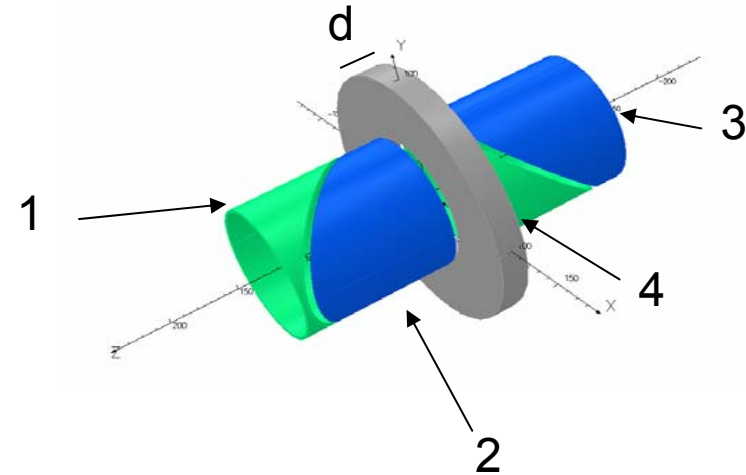
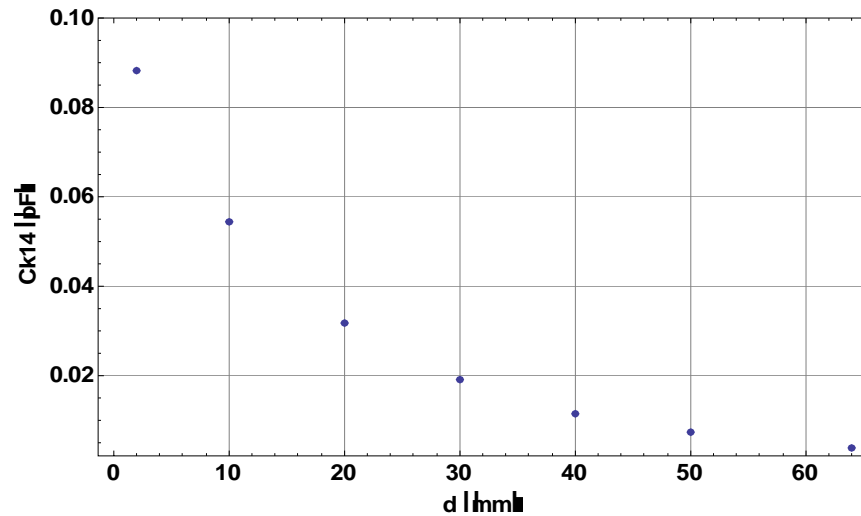
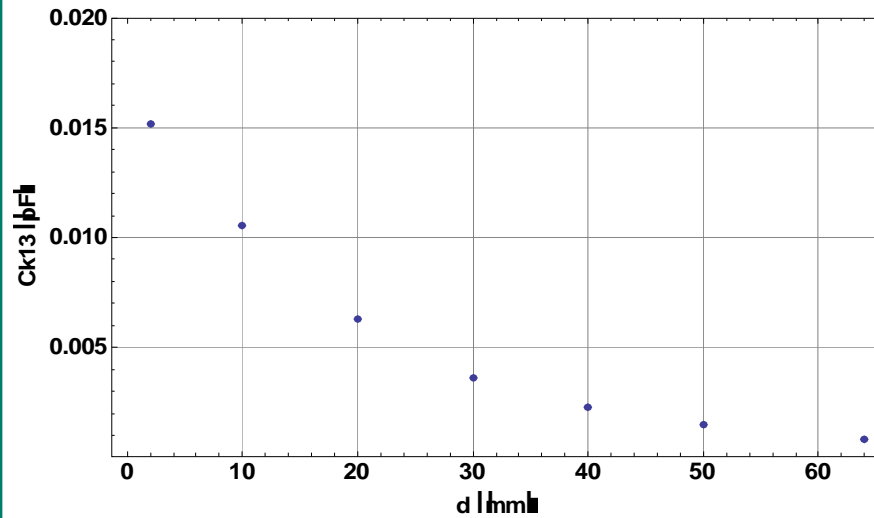


- Testet two relay changers in liquid nitrogen -> switched for >150 10⁶ times.
- Switching power changed from 32 mW (300 K) -> 4 mW (77 K)
- Change of On resistance over life time?
- Is through resistance the same for the two ways in a changer?

$$U_{signal} \propto \frac{1}{R_L} \rightarrow \text{RL}=20 \text{ Ohm (Q=275), comparability } 10^{-3} \\ \text{Difference of through resistance } < 0.02 \text{ Ohm}$$

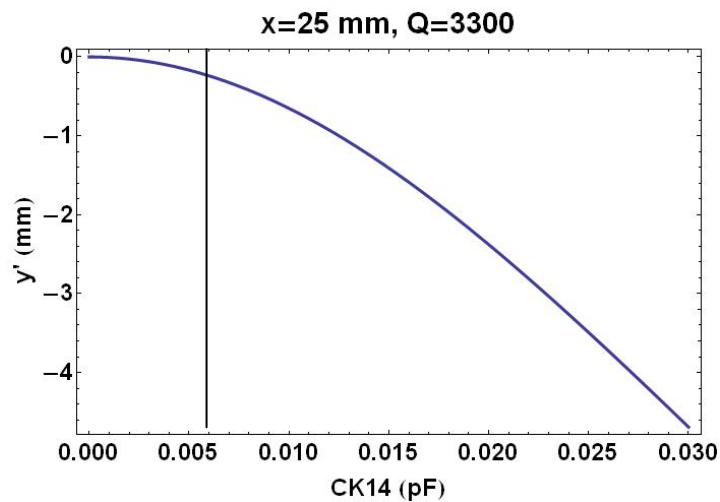
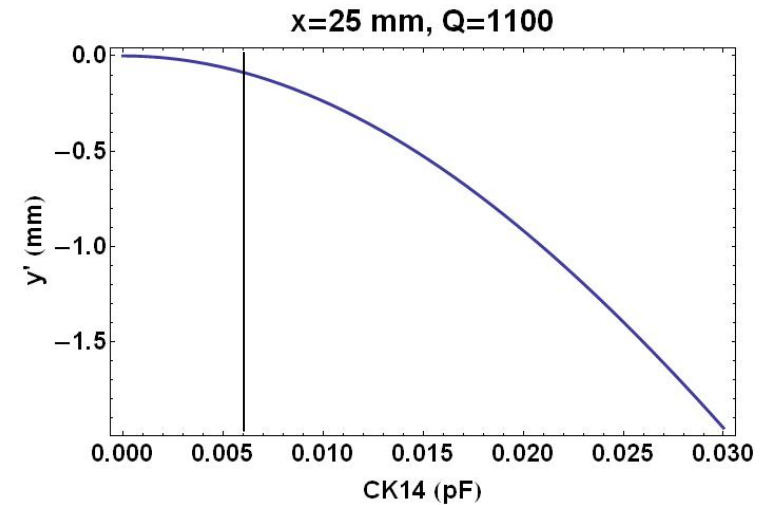
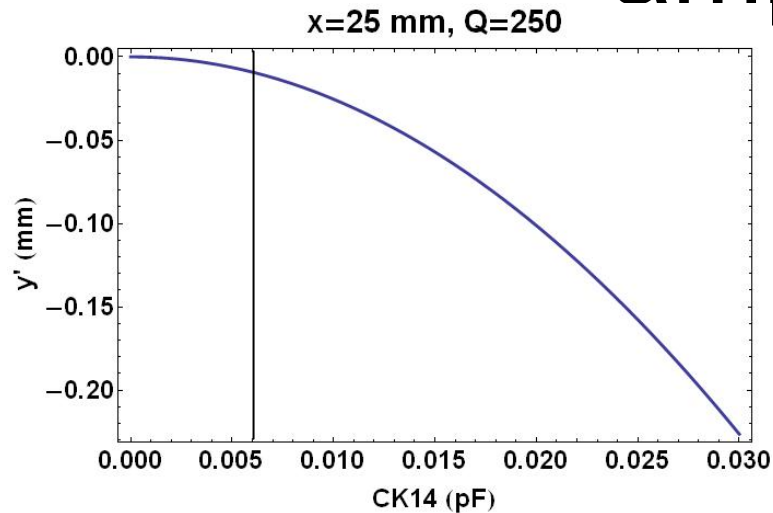


Dependence of coupling on width of middle guard ring





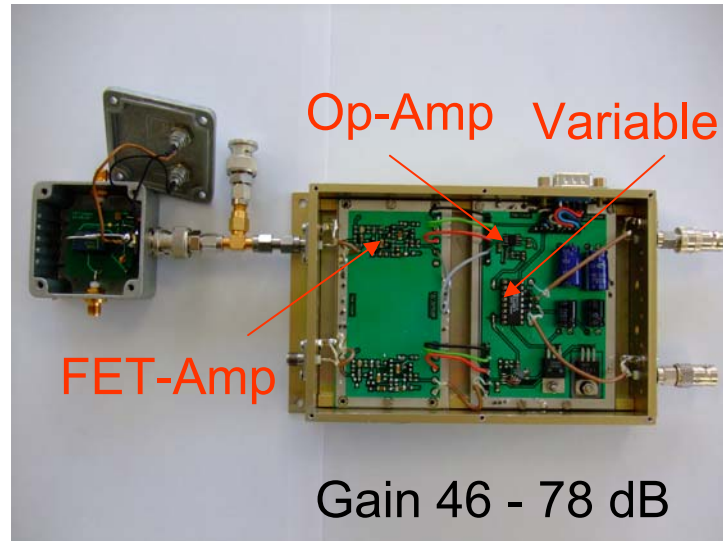
Coupling between pickups - resonant amplification



If simultaneous measurement of one electrode is required the guard ring separating one pickup from the other should have a thickness $> 6 \text{ cm}$.



Test Measurements



Op-Amp Variable gain amp

FET-Amp

Gain 46 - 78 dB

Data acquisition with SiS3300
14 bit ADC,
 $f_{\text{sampling}} = 80 \text{ MHz}$,
average over 4800
periodes

Noise measurement

$$E_{ni}^2 = U_n^2 + E_n^2 + I_n^2 R_s^2$$

$$I_n \sim 150 \text{ fA}/\sqrt{\text{Hz}}$$

$$E_n \sim 3 \text{ nV}/\sqrt{\text{Hz}}$$

$$R_n = 20 \text{ k}\Omega$$



$$L = 19.9 \mu\text{H}$$

$$R_L = 3.3 \Omega$$

$$Q = 116 @ f_0 = 3,056 \text{ MHz}$$

$$Z(\omega_0) = 44.2 \text{ k}\Omega$$

C^{6+} beam, $f_0 = 509.33 \text{ kHz}$, $h = 6$,
 $C_0 = 55 \text{ m}$, $l = 0.08 \text{ m}$

$$\Delta x < 0.5 \text{ mm} \rightarrow S/N \geq 520$$

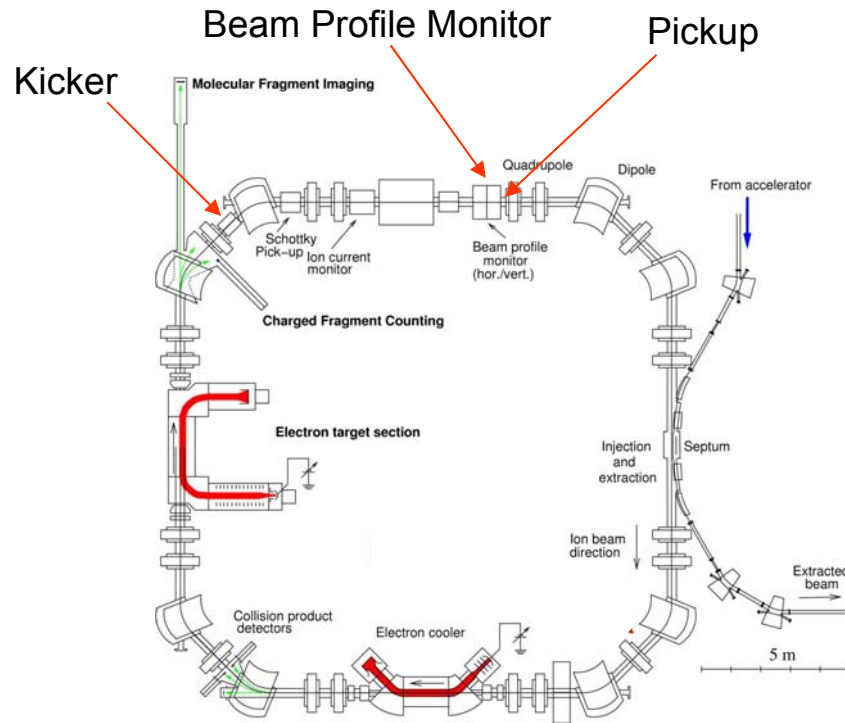
Minimum current ($\Delta f = 625 \text{ Hz}$):

- resonant: $I_b = 0.1 \mu\text{A}$
- non-resonant: $I_b = 1.7 \mu\text{A}$

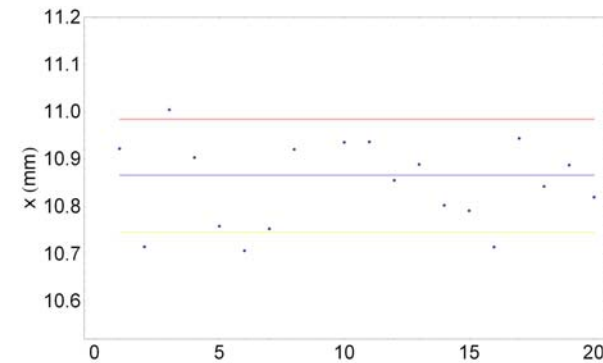
S/N improvement: 18 dB



Test Measurements

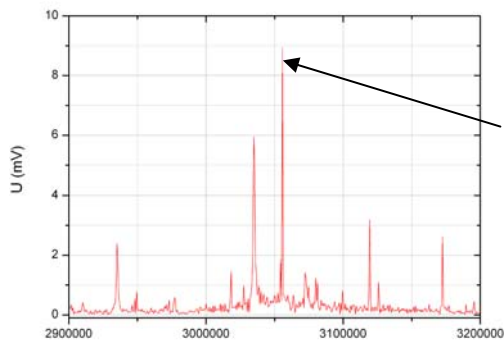


C^{6+} beam, $f_0=509.33$ kHz, $h=3$,
 $C_0=55$ m, $l = 0.08$ m, No. of measurements $N=20$



Results:

- Current: $I_b = 0.5 \mu A$
- $\bar{x} = 10.86$ mm
- $\Delta\bar{x} = 0.03$ mm
- Measured Standard Deviation: $s = 0.12$ mm
- Calculated Standard Deviation: $s = 0.07$ mm
- Calculated Standard Deviation for non-resonant amplification: $s = 1.2$ mm



$$U_{\text{kicker crosstalk}} \hat{=} I_b = 0.04 \mu A \quad (h = 6)$$



Thank you for listening!

And many thanks to the
CSR team for support!

